# **REACH – SULFIDATION & SPIKING SUMMARY**

### **SULFIDATION**

Organosulfur chemicals are the preferred reagents for catalyst sulfidation. These compounds improve initial catalyst activity and lengthen production cycles for NiMo, CoMo, NiW and CoW hydrotreating catalysts. It is the H2S formed when the chemical reaction between DMDS and H2 occurs that is responsible for the conversion of the metal in the catalyst from the oxide state to the sulphided state. This latter state is the active form.

Many Sulphur compounds can be used (EM, TBM, DMS, TNPS 537, TBPS 454) but today DMDS is the most popular choice.

The general reaction chemistry is:

 $R-S-R + H2 \rightarrow H2S + 2 R-H$ 

Therefore for DMDS we have:

# CH3-S-S-CH3 + 3H2 $\rightarrow$ 2H2S + 2CH4 (methane)

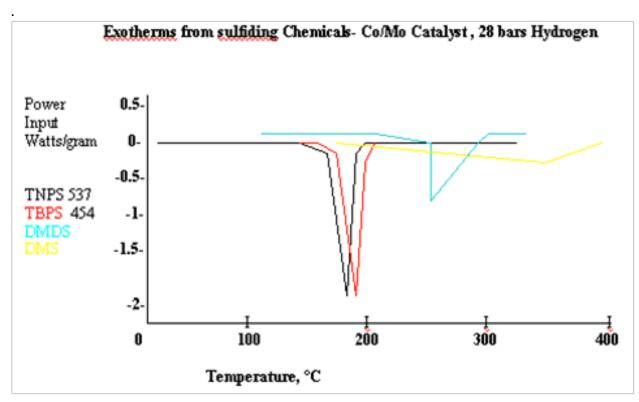
Then the conversion of the metal in the catalyst to the metal oxide (active) form in the catalyst:

 $MeO + H2S \rightarrow MeS + H2O$ 

Typically:

MoO₃ NiO₃ WO3 CoO3	H <sub>2</sub> S + H <sub>2</sub> —>	MoS <sub>2</sub> Ni <sub>3</sub> S <sub>2</sub> WS <sub>2</sub> Co <sub>9</sub> S <sub>8</sub>	
Metal	Oxide	Sulfide I	H <sub>2</sub> S required/mole metal
Мо	MoO <sub>3</sub>	MoS <sub>2</sub>	2 mole
96	96+(3x16)=144	96+(2x32)=160	2x{(2x1)+32)}=68
W	WO <sub>3</sub>	WS <sub>2</sub>	2 mole
184	184+(3x16)=232	184+(2x32)=248	2x{(2x1)+32)}=68
Ni	NiO <sub>3</sub>	$Ni_3S_2$	2/3mole
59	59+(3x16)=107	1/3x{(3x59)+(2x32)}=80	$2/3x{(2x1)+32}=22.7$
Со	CoO	Co <sub>9</sub> S <sub>8</sub>	8/9mole
59	59+16=75	1/9x{(9x59)+(8x32)}=87	.4 8/9x{(2x1)+32)}=30.2

\* atomic masses to nearest whole number



i.e. 96 (g/kg/lb) Mo equivalent to 144 (g./kg./lb.)oxide forms 160 (g./kg./lb.) sulfide which requires 68 (g/kg/lb)  $H_2S$ 

## SPIKING

The manufacture of olefins such as ethylene, propylene and higher types by thermal cracking of hydrocarbons in presence of dilution steam in tubular reactors and its economics are greatly affected by undesired side reactions. These side reactions, among which are coke and CO formation, reduce the olefins yield and limit equipment performance. Tube metallurgy and operating conditions severity are known to influence both CO and coke. A variety of chemicals are added to feedstock or dilution steam streams to help control coke and CO formation.

Many Sulphur compounds can be used (EM, TBM, DMS, TNPS 537, TBPS 454) but today DMDS is the most popular choice.

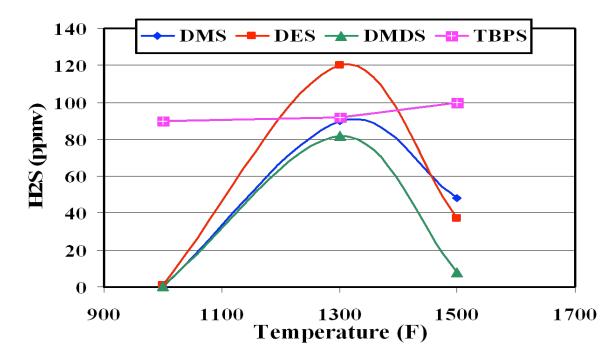
The chemistry is the same as for Sulfidation:

 $\text{R-S-R} + \text{H2} \rightarrow \text{H2S} + 2 \text{ R-H}$ 

Therefore, for DMDS we have:

CH3-S-CH3 +  $3H2 \rightarrow$  2H2S + 2CH4 (methane)

The sulphur from the H2S is used to protect the metallurgy and help inhibit the formation of coke.



### **GENERAL INFORMATION FOR SULFIDATION AND SPIKING**

If the reaction of DMDS in a hydrogen rich environment were to give 100% theoretical yield of H2S and methane, the stoichiometry is as follows:

(DMDS)CH3-S-S-CH3+ $3H2 \rightarrow$ 2H2S +2CH4 (methane)(1 mole)12+(3x1)+(2x32)+12+(3x1)=943 mole H22 mole H2S2 mole CH4

S content DMDS is (2x32)/94x100=68% ; 94/2 or 47 g. required per mole of H2S 3/2 or 1.5 mole H2 required per mole of H2S 2/2 or 1.0 mole hydrocarbon (methane) produced per mole H2S

Then 42.72 kgs of DMDS would give 14.54 kgs of CH4 and 30.90 kgs of H2S.

Various methods may be used for the disposal of spent caustic including incineration; sending to a flare from a wet oxidation process or, using a biochemical process. This will depend on the designer of the unit. For example, if this is ADNOC then this is an ethane cracker designed by Linde, so  $H_2S$  is almost completely removed in the caustic tower and final disposal is by a spent caustic handling system.

The possible reactions in a caustic tower are:

2NaOH	+ H <sub>2</sub> S	$-> Na_2S + 2H_2O$
NaOH	+ H <sub>2</sub> S	-> NaHS + H <sub>2</sub> O
$Na_2S$	+ $H_2S$ + $H_2O$	—> 2NaHS
NaHS	+ $H_2S$ + NaOH	-> 2NaHS + H <sub>2</sub> O

The resulting spent caustic typical composition is:

<u>Composition</u>	<u>Wt %</u>				
Na <sub>2</sub> CO <sub>3</sub> Na <sub>2</sub> S/NaHS NaOH NaRS NaCl Dissolved H/C Phenol Cyanides H2O	1 - 8 0 - 3.5 1.5 - 2.5 0.0 - 0.2 0.0 - 0.05 0.0 - 0.04 0.0 - 0.025 0.0 - 0.05 Balance				

If incineration is used for spent caustic disposal, the fate of the  $H_2S$  depends on the temperature of incineration. In USA it is not possible to incinerate as it is required to have more than 98% destruction. The preferred method of disposal of the spent caustic is wet oxidation. Sulfides must be converted by oxidation to sulfates or thiosulfate or by neutralization to hydrogen sulfide gas, which may be sent to a sulfur recovery plant, be reused or be burned in the flare.

If oxidation is used in the spent caustic handling process, then

NaHS	+	20 <sub>2</sub> +	NaOH	->	$Na_2SO_4$	+	H <sub>2</sub> O		
$Na_2S$	+	2O <sub>2</sub>		->	$Na_2SO_4$				
NaRS	+	5/2 O <sub>2</sub> +	NaOH	->	$Na_2SO_4$	+	NaOOR	+	$H_2O$

There is always a small amount of  $H_2S$  generated and sent to the flare. Spent caustic wet air oxidation units operated at relatively high temperatures (greater than 240°C (or °F)) will oxidize more of the organics present in the feed. Usually organic oxidation results in breaking large molecules into smaller ones. Except for wet air oxidation units that run at extreme oxidizing conditions, most of the organics end up as simple acids (acetic acid, formic acid, etc.) or their basic counterparts (acetate, formate). The net effect of wet air oxidation is a reduction in alkalinity and COD. All CPC's plants in the USA and Middle East all have a Zimpro wet oxidation system. From CPChem's point of view, the chemical processing that takes place is the transformation of DMDS into H2S. Therefore, DMDS is regarded as an intermediate in the manufacture of H2S. This is in line with the REACH Regulation Article 3(15) and also with the Guidance Document on Intermediates version 2.0 dated December 2010. The substance H2S formed from DMDS will further react with the metals of the catalyst and any residuals of H2S will be treated as a waste.